

# PERFORMANCE EVALUATION FOR NET PYRRADIOMETERS

LU Wenhua, MO Yueqin and YANG Yun

Atmospheric Observation Technology Center, China Meteorological Administration

46 Zhongguancun Nandajie, Beijing 100081, China

Tel: 0086 10 68406866 Fax: 0086 10 68400936 E-mail: [lwh@cma.gov.cn](mailto:lwh@cma.gov.cn)

## ABSTRACT

The performance of two models Net Pyrradiometer (model DFY5 and model TBB-1) made in China has been tested. We have mainly studied the long-term stability of sensitivity, nonlinearity, temperature dependence, directional response (cosine and azimuth), response time and influence of dome-shape. Sensitivity, response time and influence of dome-shape are tested in outdoor exposure and others are tested on the laboratory test facility. Main error of Net Pyrradiometer is given according to a great of test data and analysis.

## 1. INTRODUCTION

The net pyrradiometer is intended for the analysis of the radiation balance of Solar and Far infrared radiation, i.e. the net pyrradiometer is used to measure the differences of irradiance between downward and upward radiation including downward short-wave radiation, downward long-wave radiation, upward short-wave radiation and long-wave radiation. There are 50 radiation observation stations used two models Net Pyrradiometer (model DFY5 and model TBB-1) made in China to measure the net irradiance since 1990. The principle of instrument is a thermopile detector equipped with polyethylene domes and the voltage output is divided by the sensitivity to obtain irradiance. In order to evaluate the net pyrradiometers performance we have tested the main specifications. Main error for net pyrradiometers are concluded according to a great of test data and analysis.

## 2. PERFORMANCE TEST

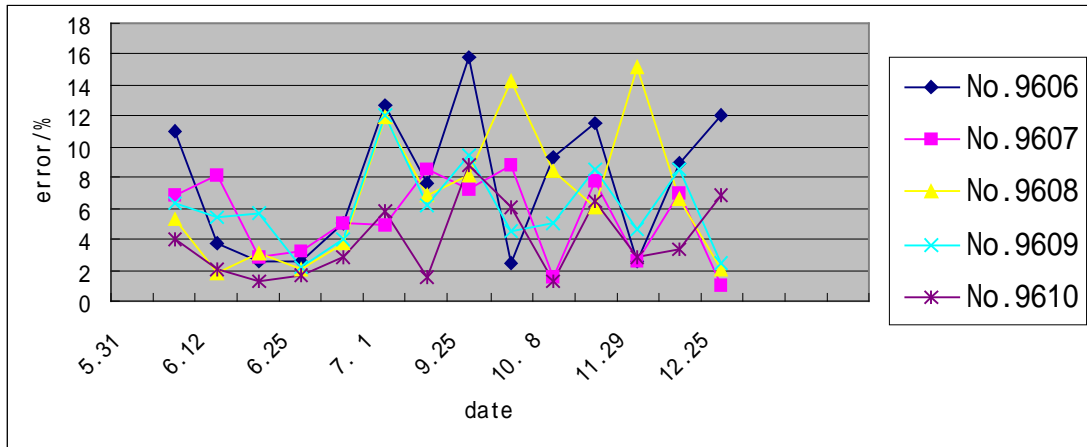
Nine instruments are tested, which serial numbers are 007, 008, 015, 047 for model DFY5 and 9606, 9607, 9608, 9609, 9610 for model TBB-1. In the measurements we use a PC in conjunction with data logger and output of instrument can be measured and processed automatically.

### 2.1 Sensitivity and Long-term Stability

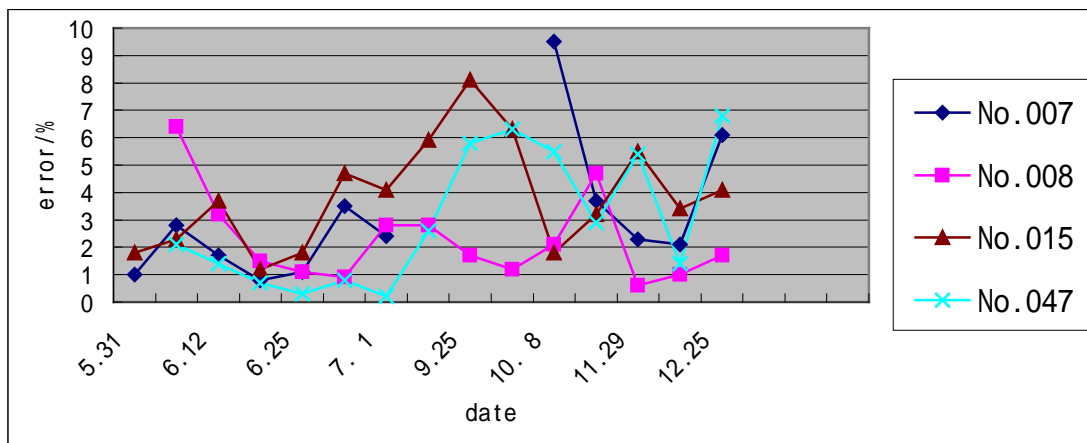
Net pyrradiometer No.84001 ( model CN-11, from EKO Japan) is used as a reference instrument. The test and reference instruments are put on the platform of roof. Data are collected every two minutes. Sensitivity is tested in different seasons and weather condition (clear day, nebulous, cloudy and less than 5 m/s wind speed). From the measurements we have got two sensitivity for the net pyrradiometer. That is daytime sensitivity (total-wave sensitivity) and nighttime sensitivity (longwave sensitivity).

The experiment is covered 8 months and the results are given in Fig.1, Fig2,

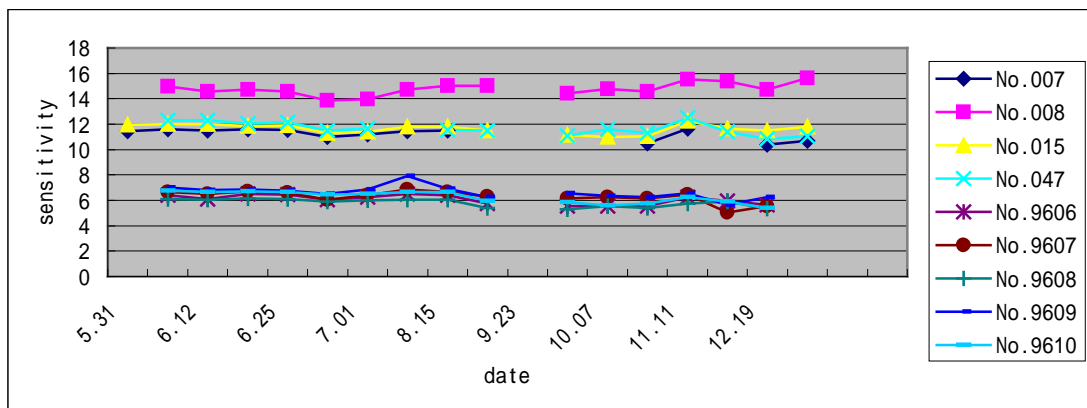
Fig3 and Fig4. It shows that the daytime sensitivity is very dispersed which occurs at the condition of lower solar elevation angle(less than  $30^\circ$ ) and lower temperature (less than  $0^\circ\text{C}$ ). The maximum relative error is about 16% for model TBB-1 at the daytime. This is a combined error caused by nonlinearity, temperature dependence, directional response, zero drift of the instrument and et al.



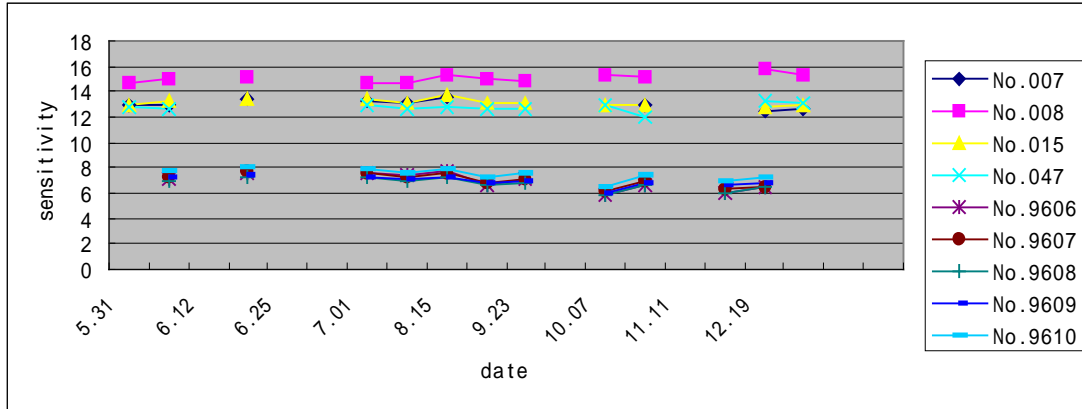
**Fig 1. Daytime Sensitivity Change for Model TBB-1 Net Pyrradiometer**



**Fig2. Daytime Sensitivity Change for Model DFY5 Net Pyrradiometer**



**Fig 3. Long-term Stability of Daytime Sensitivity over 8 Months**



**Fig 4. Long-term Stability of Nighttime Sensitivity over 8 Months**

Nonlinearity is tested in the laboratory. The test facility consists of mechanism and a solar simulator that the spectrum components do not change with irradiance. Test point is respectively at irradiance of 250, 500, 750 and 1000 W/m<sup>2</sup>. Nonlinearity is given by  $\delta_L = (V/V_{500} - 1) \times 100\%$ . In the formula V is the output of net pyrradiometer and V<sub>500</sub> is the output of net pyrradiometer when the irradiance is 500W/m<sup>2</sup>. From the results we know that the maximum nonlinearity error is 2.3% and is in the lower irradiance.

### 2.3 Temperature Dependence

Temperature dependence is tested on the laboratory test facility with a temperature chamber. We change the temperature in the chamber while the irradiance is unchanged and then the output of instrument is measured. The temperature test point is respectively at -20°C, 0°C, 20°C, 40°C while the irradiance is 1000W/m<sup>2</sup>. Temperature error is given by  $\delta_T = (V_T/V_{20} - 1) \times 100\%$ . In the formula V<sub>T</sub>, V<sub>20</sub> is respectively output of instrument when the temperature is T and 20°C. From the results the temperature error is within  $\pm 5\%$ .

### 2.4 Directional Response

Directional response can be divided into cosine response and azimuth response

#### 2.4.1 Cosine Response

Cosine response test is made use of studying the directional character of incident beam. The irradiance is adjusted to 1000 W/m<sup>2</sup> on the laboratory test facility. First the output of instrument (V<sub>0</sub>) is tested in  $\theta = 0^\circ$  ( $\theta$  is zenith angle), namely solar elevation angle  $h = 90^\circ$ , then the solar elevation angle  $h$  is adjusted to  $80^\circ$  to measure the output of instrument. Each angle of measurement is at  $90^\circ$ ,  $80^\circ$ ,  $70^\circ$ ,  $60^\circ$ ,  $50^\circ$ ,  $40^\circ$ ,  $30^\circ$ ,  $20^\circ$ ,  $10^\circ$ . The output of instrument for solar elevation angle  $90^\circ$  ( $\theta = 0^\circ$ ) is tested again.

Cosine response error is calculated by formula  $\delta_\theta = (V_\theta/V_i - 1) \times 100\%$ . In the formula the relation between  $\theta$  and  $h$  is  $h = 90^\circ - \theta$ , V<sub>θ</sub> is the output of instrument at  $\theta$ , and V<sub>i</sub> = V<sub>0</sub> · cos  $\theta$  is an ideal value at  $\theta$  and V<sub>0</sub> is the average of two outputs of

instrument at  $\theta=0^\circ$  . The results are listed in the table 1. The maximum error is 15.65% at solar elevation angle  $10^\circ$  .

**Table 1. The Relative Error for Cosine Response ( % )**

No.	Model	$10^\circ$	$20^\circ$	$30^\circ$	$40^\circ$	$50^\circ$	$60^\circ$	$70^\circ$	$80^\circ$
007	DFY5	-15.65	-9.02	-4.67	-2.96	-1.88	-1.33	-0.01	0.29
008	DFY5	-15.62	-7.80	-4.29	-1.35	-0.41	0.21	0.47	0.41
015	DFY5	-3.93	-0.43	0.57	0.80	0.29	-0.02	0.25	0.57
047	DFY5	-7.53	-2.98	0.42	0.37	0.14	-0.08	0.86	0.70
9606	TBB-1	0.39	-0.39	0.06	-0.51	-0.35	-1.17	-1.98	-1.88
9607	TBB-1	-1.62	-3.39	-3.79	-2.42	1.34	2.38	1.77	0.63
9608	TBB-1	5.19	2.85	1.57	-0.51	-0.43	-0.24	-0.81	-0.87
9609	TBB-1	-7.68	-3.71	2.27	-1.48	-0.45	-0.79	-0.90	-1.14
9610	TBB-1	2.33	-2.25	-0.16	-0.39	-0.01	0.19	0.19	-0.63

#### 2.4.2 Azimuth Response

The method of azimuth response test is similar to the cosine response test. The output is measured at solar elevation angle  $10^\circ$  . The test point is at intervals of  $30^\circ$  within directional  $60^\circ \sim 300^\circ$  . The cable of net pyrradiometer points to north which is  $0^\circ$  .

**Table 2. The Relative Error for Azimuth Response ( % )**

No	Model	$300^\circ$	$270^\circ$	$240^\circ$	$210^\circ$	$180^\circ$	$150^\circ$	$120^\circ$	$90^\circ$	$60^\circ$
007	DFY5	-7.63	1.78	0.63	5.65	-4.96	5.94	3.07	1.12	-5.60
008	DFY5	5.34	5.16	-14.52	5.30	2.41	1.26	-4.95	3.85	5.90
015	DFY5	8.81	10.98	0.71	3.72	-20.07	-4.10	0.74	1.32	-2.11
047	DFY5	1.96	4.32	2.56	3.87	-19.70	4.86	-0.08	4.01	2.42
9607	TBB-1	-1.25	0.34	-3.39	-2.03	-0.67	-1.08	5.85	6.53	4.31
9608	TBB-1	-10.43	2.97	11.42	10.92	2.74	-0.38	-5.45	-11.72	-10.50
9609	TBB-1	-2.52	2.40	-1.68	-4.32	1.94	1.11	-0.88	14.92	-10.97
9610	TBB-1	-9.21	-3.63	0.31	-0.85	4.08	6.91	1.99	2.21	-1.82

Azimuth response error is given by the formula  $\delta_A=(V_Z/V_M-1)\times 100\%$  .  $V_Z$  is the output of each azimuth and  $V_M$  is an average of outpoints for all azimuth. The results are given in the table 2. It shows that the error of azimuth response is in  $-20,07\% \sim 14.92\%$  . According to the observation condition in use we should test 6 points, namely  $60^\circ$  ,  $90^\circ$  ,  $120^\circ$  ,  $240^\circ$  ,  $270^\circ$  ,  $300^\circ$  and its error should be less than 15%. Pay attention to that the direction of net pyrradiometer must be the same

whether in the test or in the observation, i.e. the cable of net pyrradiometer points to north.

### **2.5 Response Time**

The response time is tested in both indoor and outdoor. The results are less than 90 second (99% response).

### **2.6 Influence of Dome-shape**

The Influence of Dome-shape is tested on the laboratory test facility which the irradiance is adjusted to 500 W/m<sup>2</sup>. According to the results maximum relative error of dome-shape is about 3%.

## **3.CONCLUSION**

Based on our test study, we conclude that for net pyrradiometers of model DFY-5 and TBB-1, there are daytime sensitivity and night sensitivity which is within 5~16  $\mu\text{V} \cdot \text{W}^{-1} \cdot \text{m}^2$ , nonlinearity error is less than 2.3%, temperature error is within  $\pm 5\%$  in the range of  $-20^\circ\text{C} \sim 40^\circ\text{C}$ , maximum cosine error is less than 16% and maximum azimuth error is less than 15% at solar elevation angle  $10^\circ$ , response time is less than 90 second (99% response) and maximum relative error of dome-shape is about 3%. Last, we want to stress that the cable of net pyrradiometer points to north and the polyethylene domes must be full of air in the observation in order to get a more accurate net radiation.

## **REFERENCES**

- WMO. Guide to Meteorological Instruments and methods of Observation. Six Edition. WMO No.8, 1996
- LU Wenhua, et al. A Laboratory Test Facility for Solar Radiation Instruments and Its Application. WMO/TD No.877, 361-364,1998.
- LU Wenhua, et al. Performance Evaluation for Pyranometers. WMO/TD No.1028, 124-127, 2000.
- LU Wenhua, et al. Study on the Calibration of net Pyrradiometer. WMO/TD No.1123, 2002.
- China Meteorological Standardization. Net Pyrradiometer QX/T 19 — 2003, Standards Press of China, 2004.