

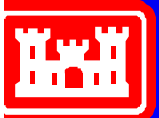
Improved Shallow-Water Wave Modeling



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Coastal and Hydraulics Laboratory

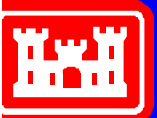


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Outline

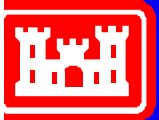
- Introduction
- Half-Plane STWAVE
- Full-Plane STWAVE
- Enhancements
 - Bottom interaction
 - Diffraction/Reflection
 - 3G Source Terms
- Summary



Global vs. Coastal

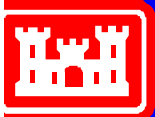


- Correct Deepwater Physics
- No Regional/Local Tuning
- Correct Shallow-water Physics



Nearshore Transformation

- Sediment Transport
- Coastal Flooding and Storm Damage
- Navigation and Harbor/Jetty Design



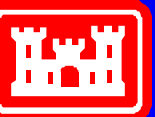
Nearshore Transformation

• Past

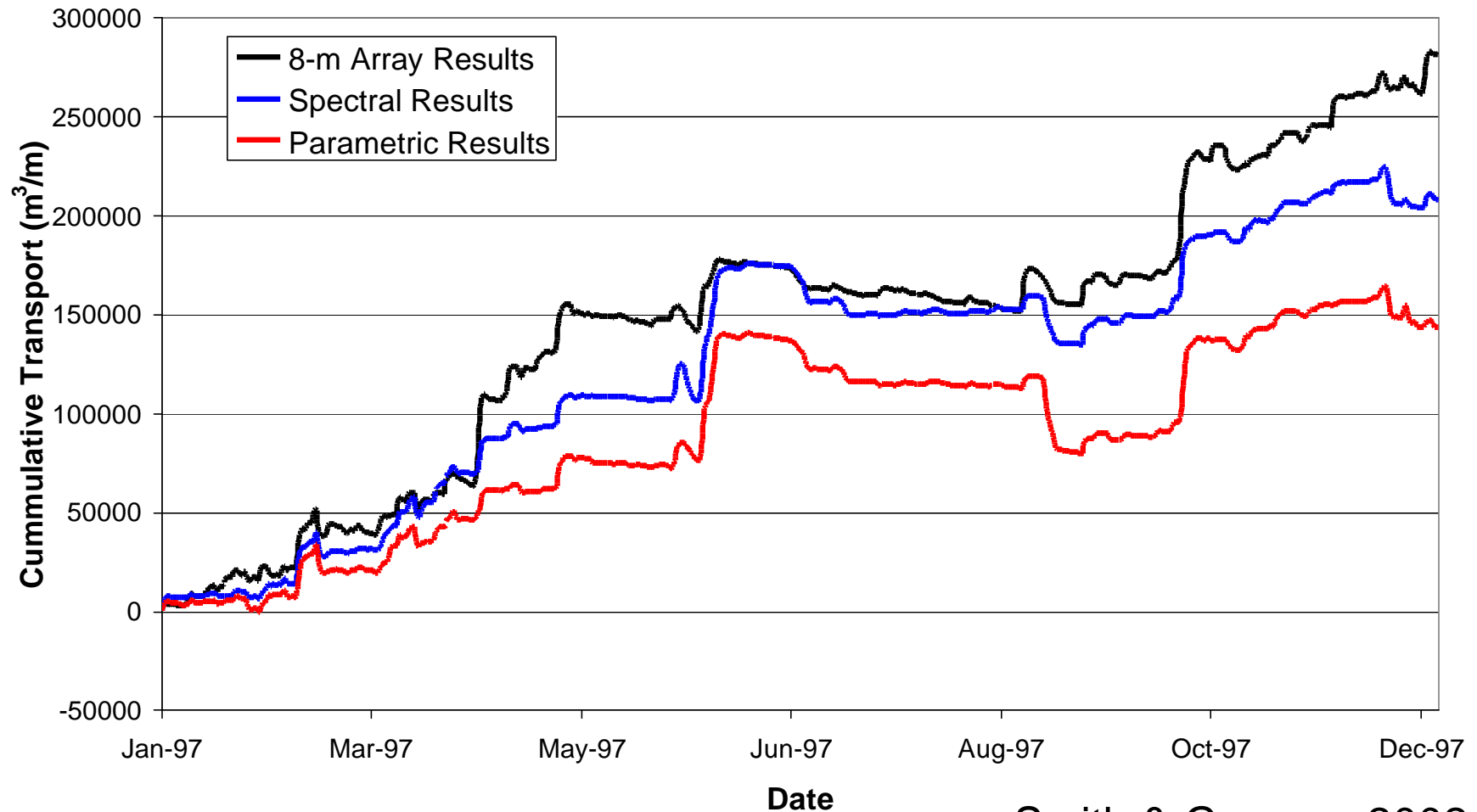
- Distribution: H , T , θ
- Climate statistics (lookup tables)
- Refraction, shoaling, and breaking

• Present/Future

- Directional spectra
 - Smith & Gravens (2002)
 - ~50% error reduction
- Full time histories
 - Interaction w/ currents & water levels
 - Update bathymetry
 - Complex spectra
- Advanced transformation processes



Longshore Transport Estimates



Smith & Gravens 2002



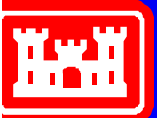
Nearshore Transformation

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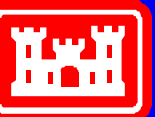


Advanced Processes

- Wave-current interaction
- Wind input
- Wave-wave interactions
- Whitecapping
- Wave-bottom interaction
- Diffraction
- Reflection
- Transmission
- Wave asymmetry

How good are present formulations in shallow water?

How many times do we need to change models for a single application?

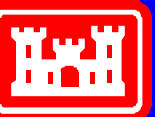


Modeling Requirements

- Grid Flexibility
- Efficiency
- Ease of Application
- Robustness

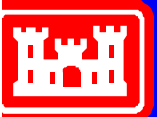
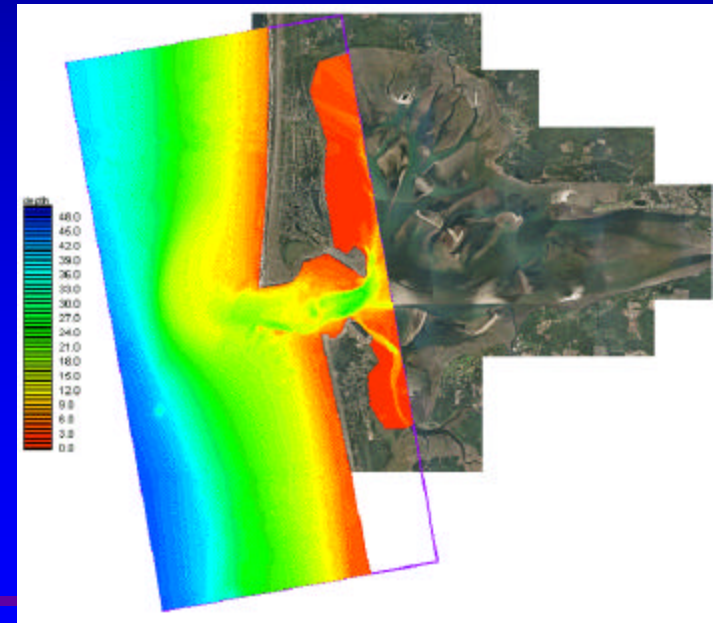


No Model Tweaking



Half-Plane STWAVE

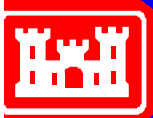
- Steady-State, Phase-Averaged
- Linear Refraction and Shoaling
- Depth and Steepness-Limited Breaking
- Linear Wave-Current Interaction
- 2G Wave Generation
- Half Plane
- Resio (1988a,b)
- Smith et al. (2001, 2002)
- Windows Interface (SMS)



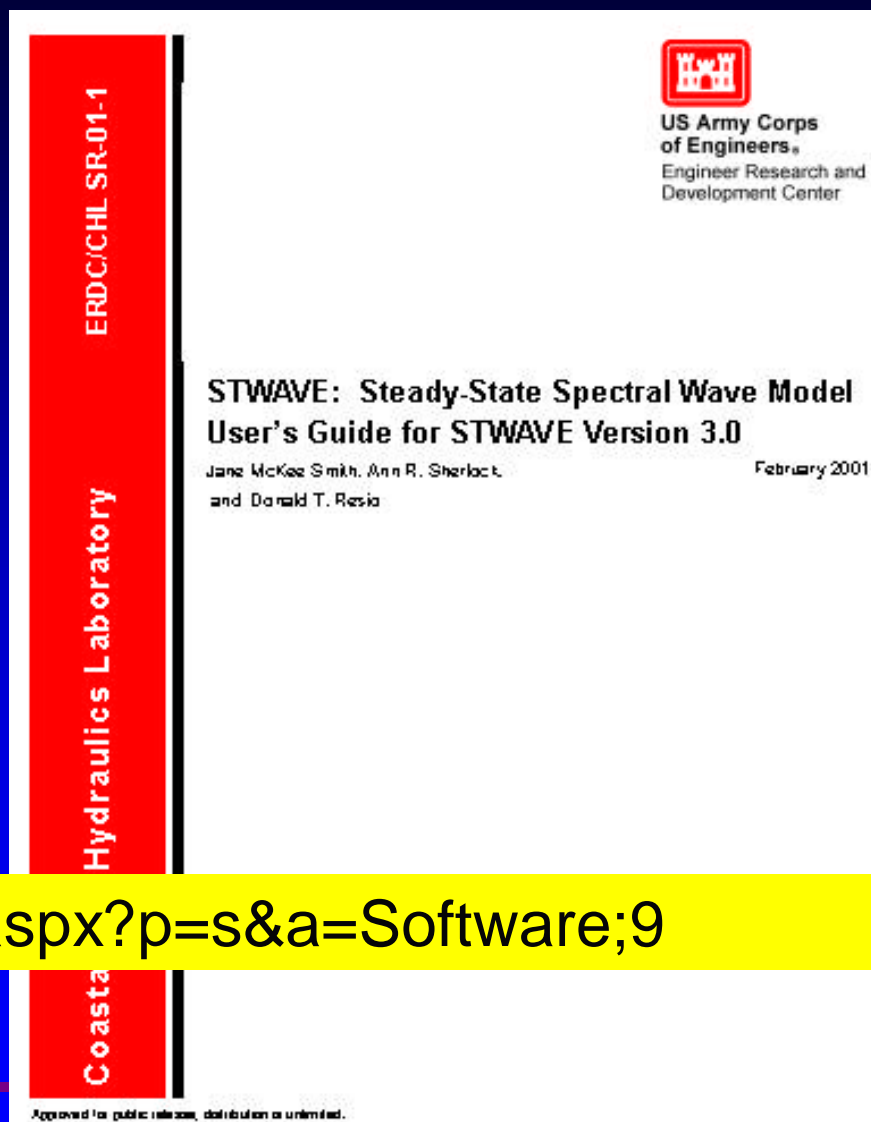
Documentation on Web

- PDF User's Guide
- Latest executable
- Sample files
- Sample applications
 - Willapa Bay
 - Grays Harbor
 - Ponce Inlet

<http://chl.erdc.usace.army.mil/CHL.aspx?p=s&a=Software;9>



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Recent Corps STWAVE Applications

Grays Harbor Entrance
Willapa Bay Entrance
Cape Shoalwater
Neah Bay

Yaquina Bay Ent
Columbia River Ent
Humboldt Bay

Camp Pendleton

Barrow

False Pass
Unalaska

Veldez
Tatitlek
Wrangell
Port Lions

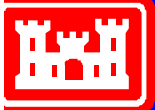
Mouth of
Colorado River
Sabine

Mobile Bay Entrance
Northern Gulf Regional
Mississippi Sound
Hurricane Georges
Pascagoula

Milwaukee Harbor Entrance

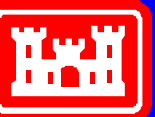
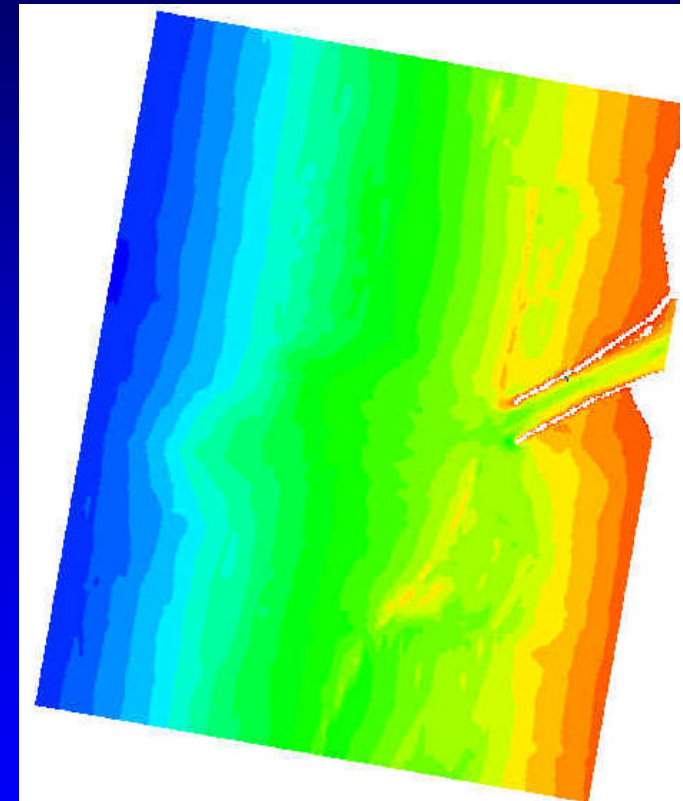
NY Harbor Entrance
Shinnecock Inlet
Long Beach
Staten Island
Hereford Inlet
Townsend Inlet
Barnegat Inlet
Ocean City, NJ
Cape May
Roosevelt Inlet
Cape Henlopen

Virginia Beach,
Chesapeake Bay
Dare County
FRF
Hurricanes Fran & Bertha
Cape Fear
Onslow Bay
Savannah
Brunswick Harbor Entrance
Ponce de Leon Inlet
Lake Worth Inlet



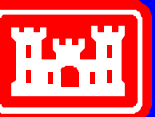
STWAVE (Half Plane) Advantages

- Substantially lower memory requirements
- Faster computational speed
- No tuning
- Benchmarked
- Robust
 - Widely used & tested
 - Parametric
- Minimal open boundary impact
- Automated nesting
- Interface (SMS) for input & output



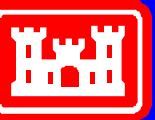
STWAVE (Half Plane) Disadvantages

- Oblique energy is lost (> 60 deg to x-axis)
- 2G physics – missing details
- Steady state
- Simplified diffraction
- Processes neglected
 - Transmission
 - Reflection
 - Bottom interactions
- Square grid cells, fixed angle bands



Full-Plane STWAVE

- **Step 1:**
Full-plane, 2G, Steady-state Model
- **Step 2:**
Bottom Interaction, Diffraction, and Reflection
- **Step 3:**
3G, Nonsteady, and 3-Wave Interactions



Full-Plane STWAVE

- Conservation of spectral action balance

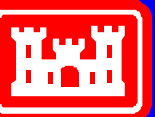
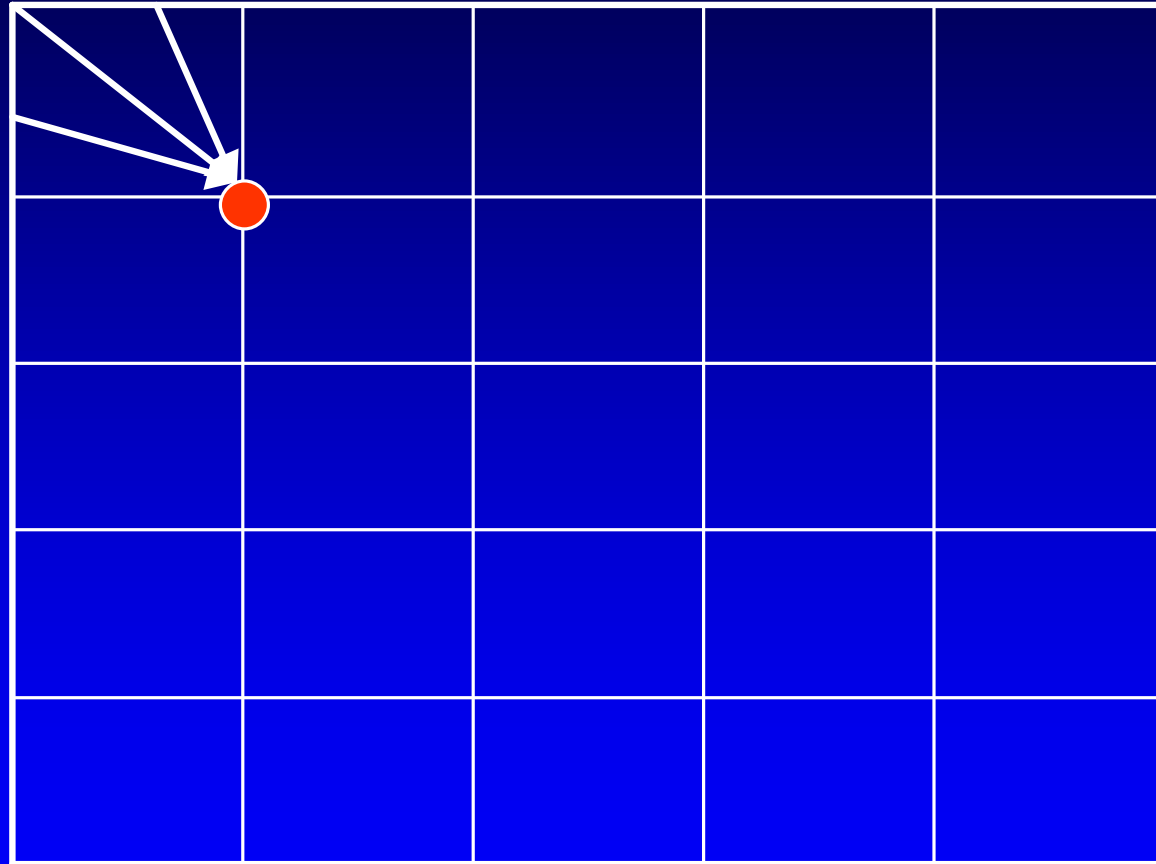
$$\begin{aligned} & (C_{ga})_x \frac{\partial}{\partial x} \frac{C_a C_{ga} \cos(\mathbf{m}-\mathbf{a}) E(f, \mathbf{a})}{w_r} + \\ & (C_{ga})_y \frac{\partial}{\partial y} \frac{C_a C_{ga} \cos(\mathbf{m}-\mathbf{a}) E(f, \mathbf{a})}{w_r} = \sum \frac{S}{w_r} \end{aligned}$$

- Back-traced wave rays



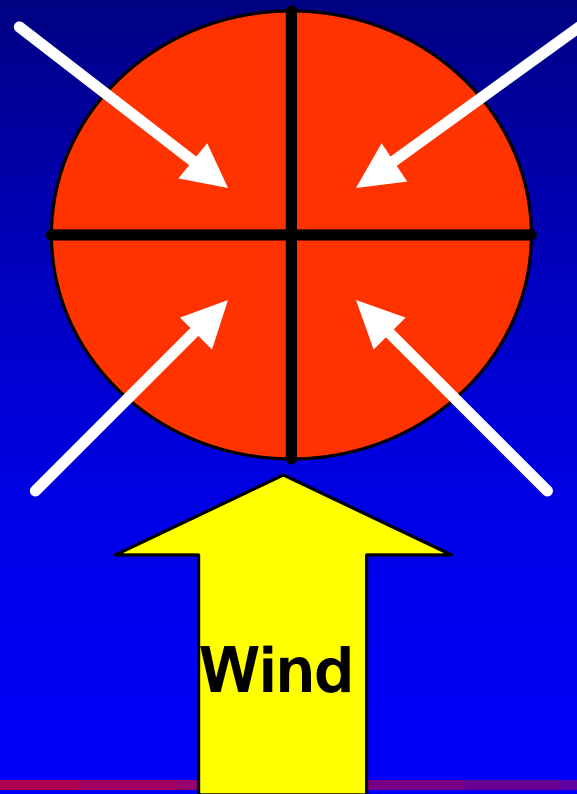
Full-Plane STWAVE

- Solved in 4 Quadrants



Full-Plane STWAVE

- Solved in 4 quadrants, alternate sweeps
- Iteration required for complex bathymetry



Full-Plane STWAVE

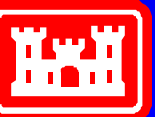
- Sources Terms

$$F_{in} = I \frac{r_a}{r_w} 0.85 C_p \frac{u_*}{g}$$

$$(f_p)_{i+1} = \left[(f_p)_i^{-3.33} + \frac{2.5 \Delta x}{g \cos(\mathbf{a})} \left(\frac{u_*}{g} \right)^{1.33} \right]^{-0.3}$$

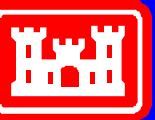
$$\Gamma_E = \frac{e g^{\frac{1}{2}} E_{tot}^3 k_p^{\frac{9}{2}}}{\tanh^{\frac{3}{4}}(k_p h)}$$

$$H_{mo_{max}} = 0.1 L \tanh kh$$



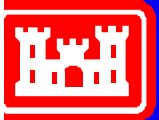
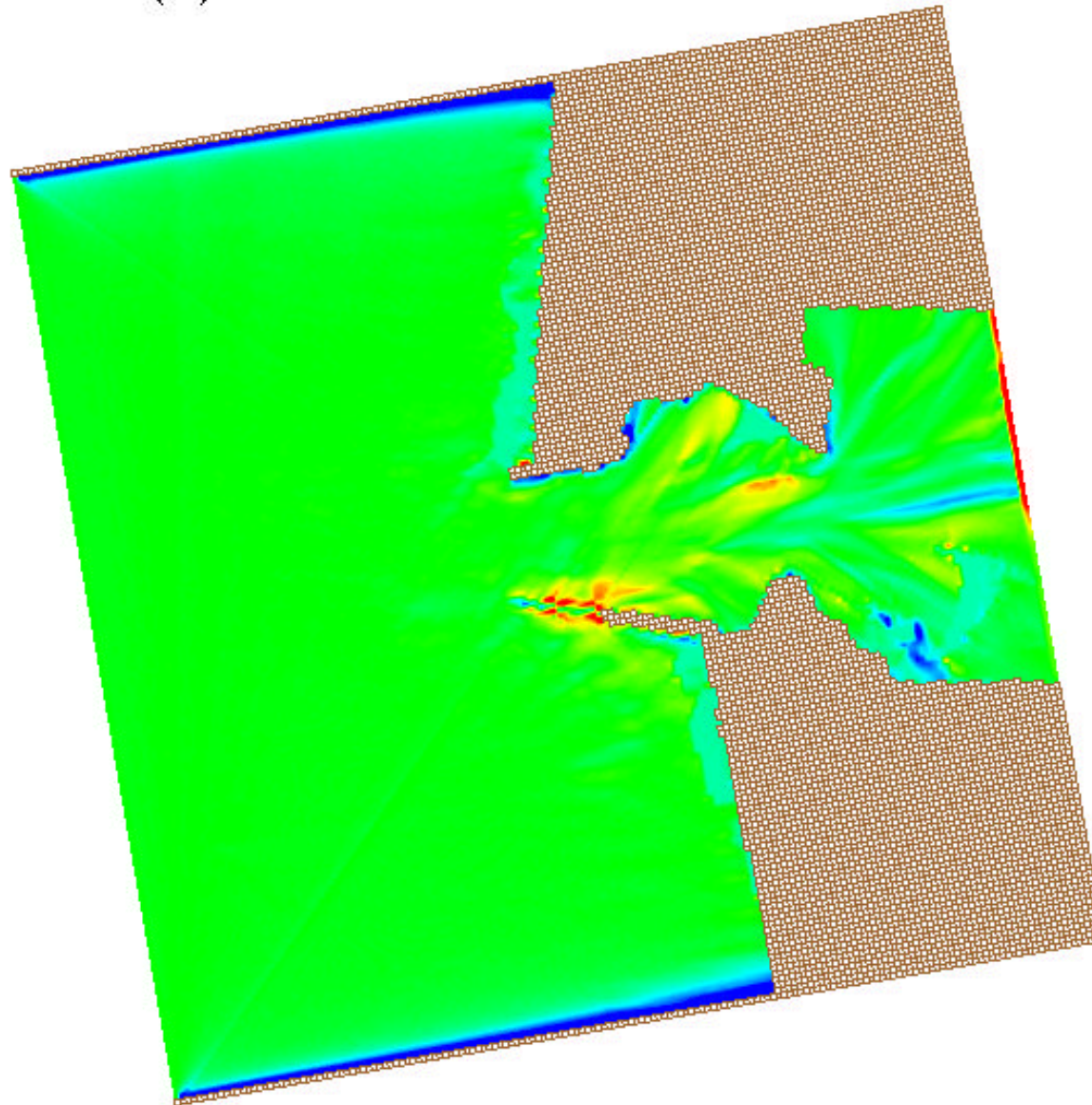
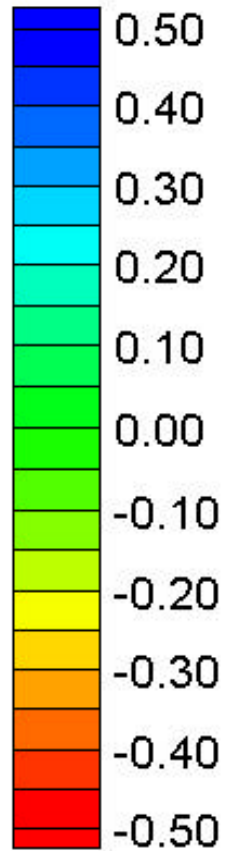
Full-Plane STWAVE

- **dx and dy not required to be equal, dq arbitrary**
- **TMA spectral generated included (H, T, q input allowed)**
- **Refraction and shoaling precomputed for efficiency (redo for tide or current variations)**



Full-Plane STWAVE

WaveHeightDifference(m)



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Diffraction and Reflection

- Diffusion operator in STWAVE + directional spread sufficient in most cases
- More rigor required for surface-piercing structures



Diffraction – Mild Slope Equation

$$\frac{1}{a} \left\{ \nabla a + \frac{1}{CC_g} \nabla a \cdot \nabla (CC_g) \right\} + k^2 - \nabla \mathbf{r} \cdot \nabla \mathbf{r} = 0$$

$$\nabla \cdot (a^2 CC_g \nabla \mathbf{r}) = 0$$

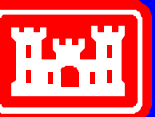
Requires high spatial resolution ($L/8$)

Solution is phase dependent

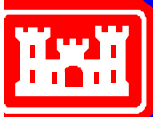
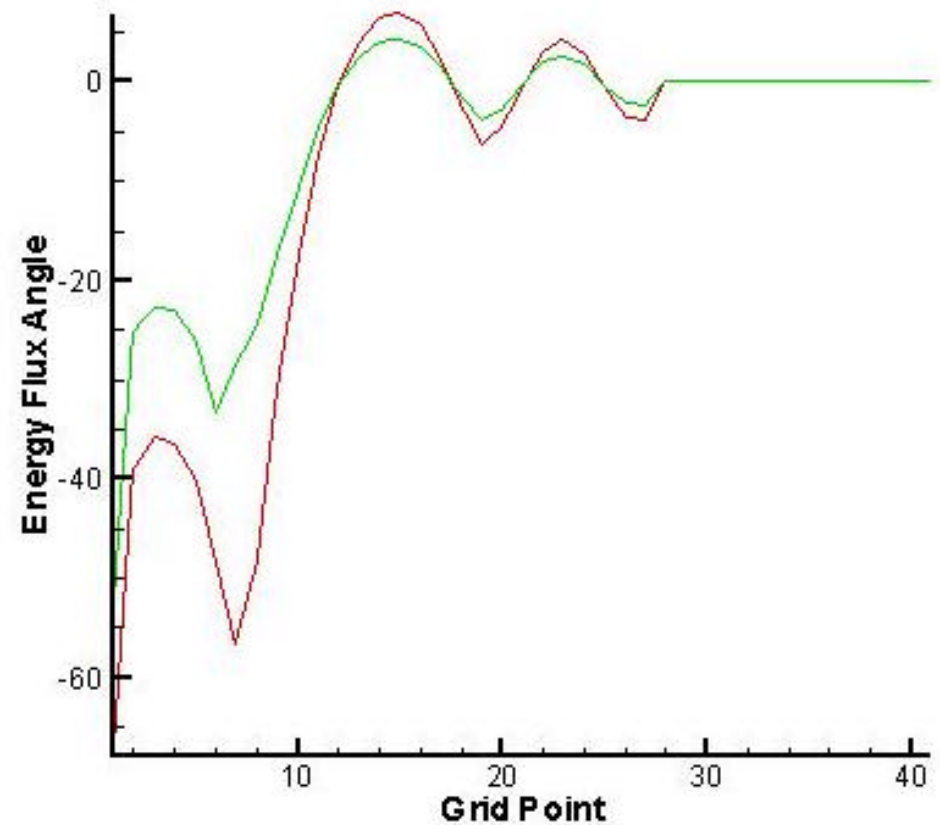
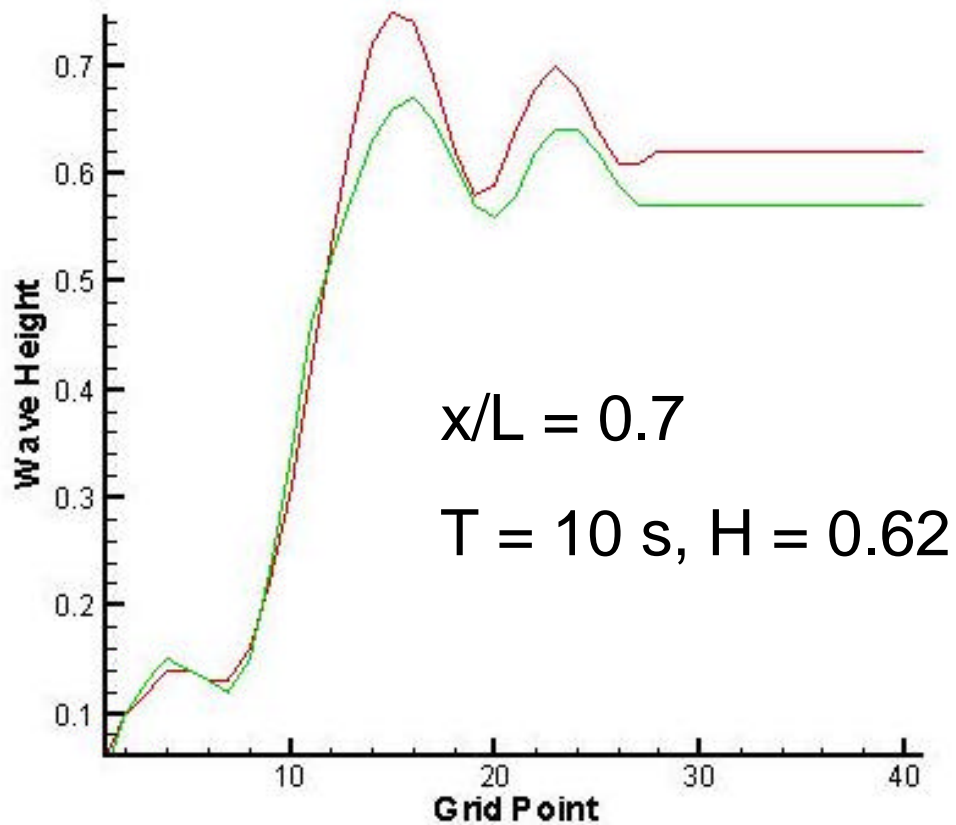


Diffraction

- Behind structure, diffraction dominates
- Solve diffraction based on geometry
 - Complex amplitude solved as integral along the boundary (Huyghens-Kirchoff integral)
 - Integrals (summations) pre-computed
 - Solution not restricted by grid resolution
- Add refraction, shoaling, and source terms

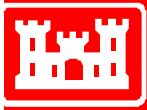
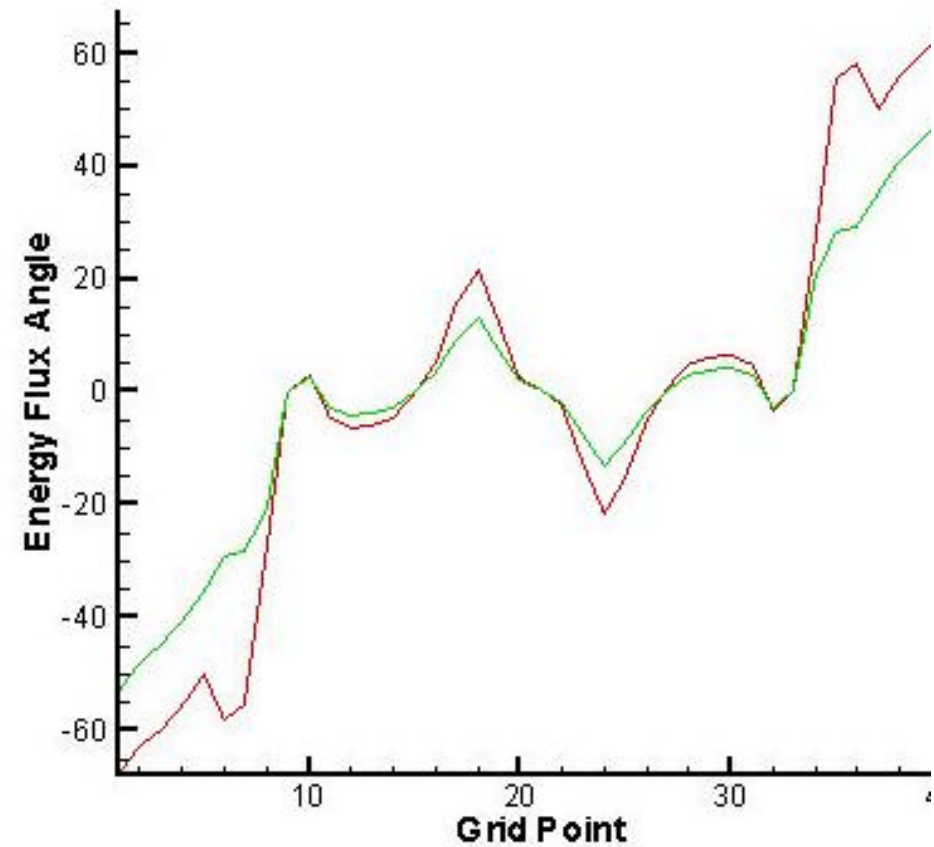
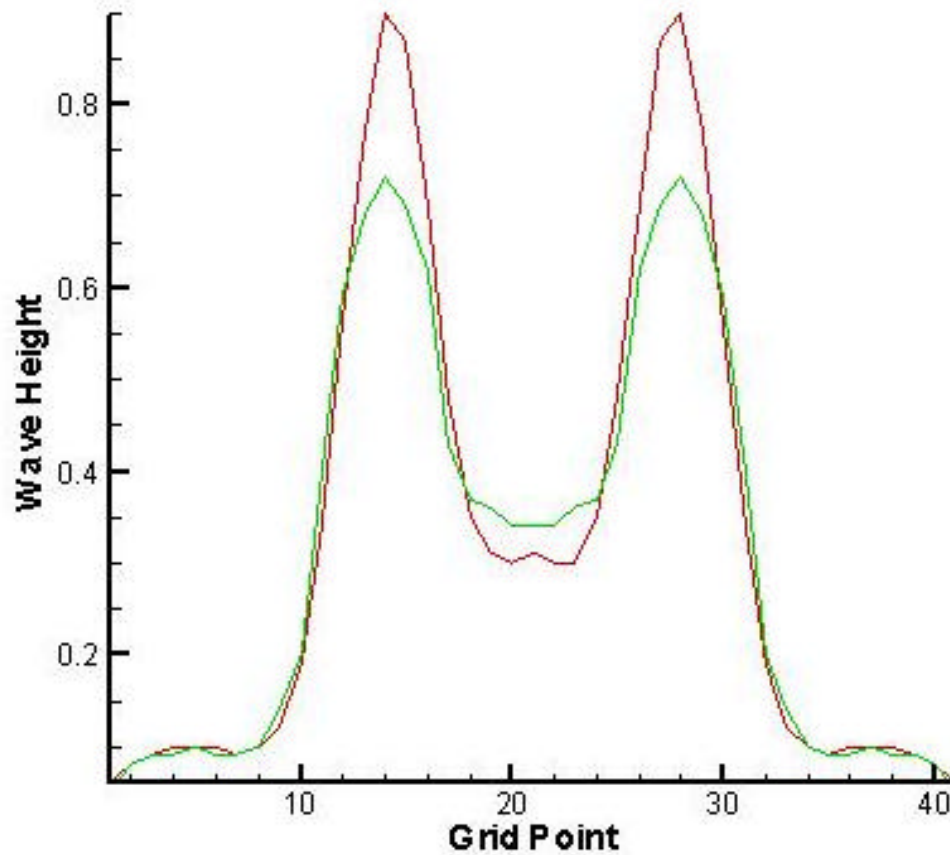


One-Arm Breakwater



Red is diffraction Only, Green is w/ refraction, shoaling and breaking

Two-Gap Breakwater



Red is diffraction Only, Green is w/ refraction, shoaling and breaking

Reflection

Apparent Aperture

Reflection coefficient = β

Reflective wall

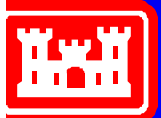
Wavelets Emitted Along y – Real Aperture

Path from single reflection

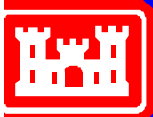
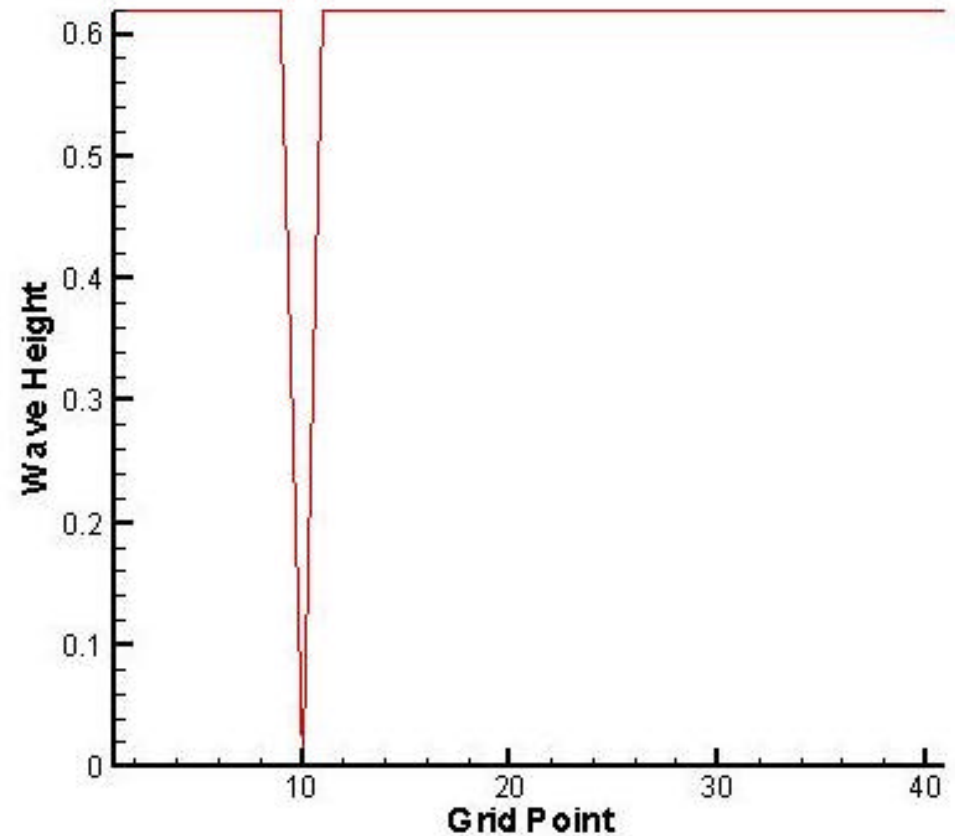
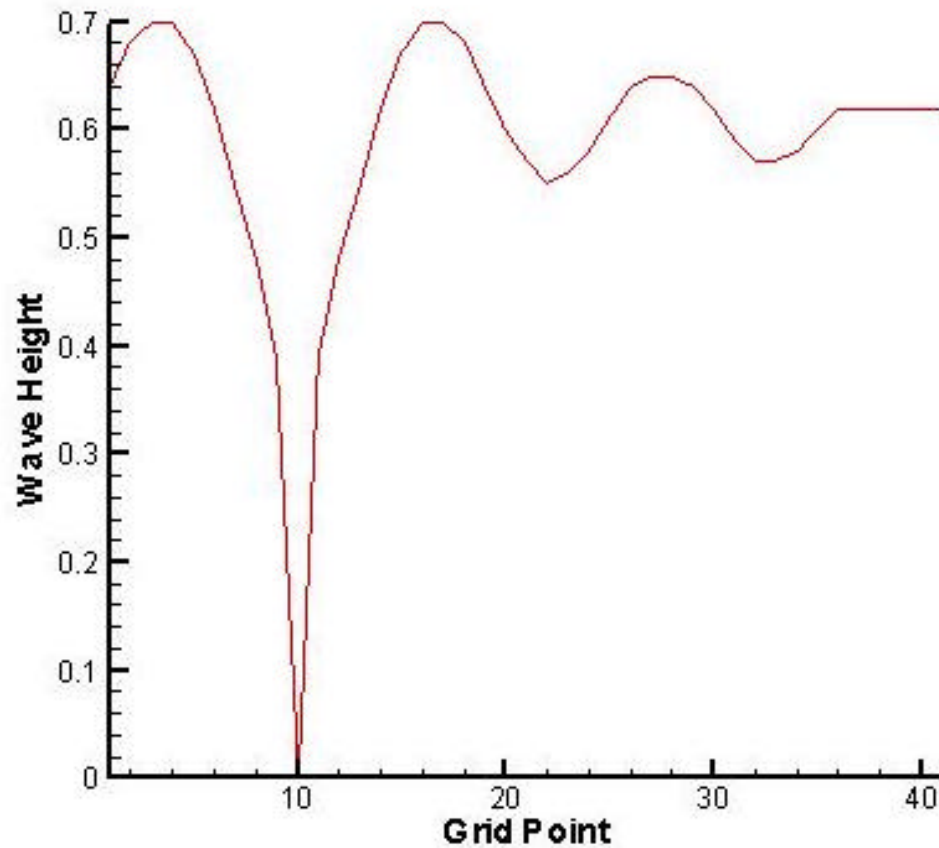
Waves propagating along “wall” are actually the sum of wavelets - same as the normal diffraction solution

Except:

$a(y)$ is multiplied by β
apparent a is mirror image

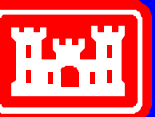


Absorbing and Reflecting Wall

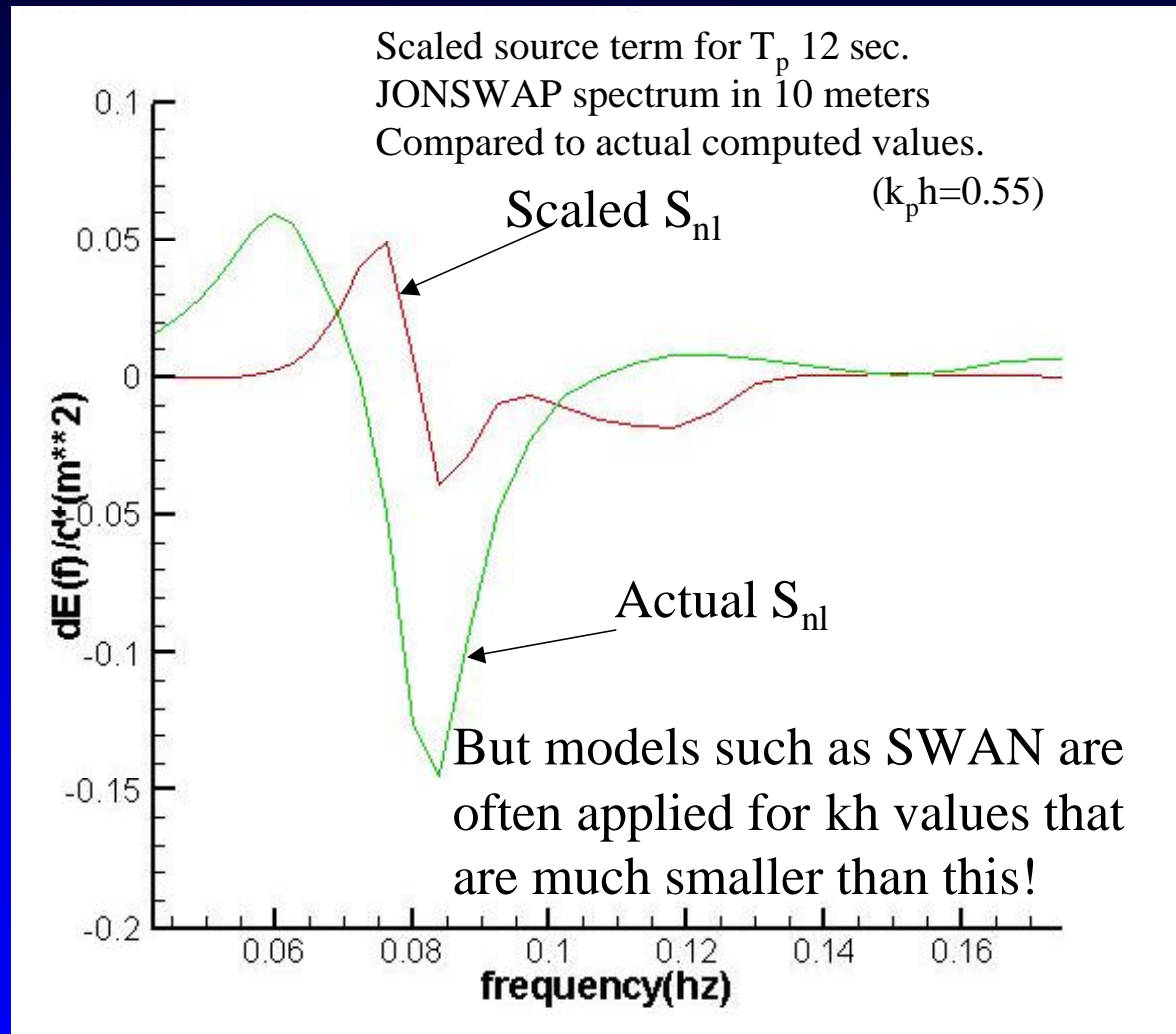


3G Source Terms

- DIA limitation in coastal regions:
 - Complex spectral shapes
 - Heterich & Hasselmann (1980) scaling $k_p h > 1$ (e.g., 10-sec wave in 20 m depth)



3G Source Terms



Summary

- **Sophisticated Nearshore Modeling Requires:**
 - Advanced physics
 - Improved efficiency and flexibility
- **On-going Effort with STWAVE**
 - Wind input function
 - High-frequency breaking
 - Arbitrary-depth wave-wave interactions
 - Incorporation of 3-wave interactions
 - Benchmarking

